Volumetric full-range magnetomotive optical coherence tomography

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1 Introduction

Magnetomotive optical coherence tomography (MM-OCT) is a variant of OCT that utilizes embedded magnetic particles within the sample to enhance imaging contrast and probe the viscoelastic properties of the sample.1,2 These magnetic particles can be engineered to target specific molecules that can enable the generation of molecular specific contrast and aid in the identification of diseased sites or organs in conjunction with MM-OCT.3,4 The goal of MM-OCT imaging is to spatially localize the presence of magnetic particles within tissues or organs. These magnetic particle-containing regions are detected by using the capability of OCT to measure small-scale displacements induced by the activation of an external electromagnet coil typically driven by a harmonic excitation signal. The constraints imposed by the scanning schemes employed and tissue viscoelastic properties limit the speed at which conventional MM-OCT data can be acquired. Realizing that electromagnet coils can be designed to exert MM force on relatively large tissue volumes (comparable or larger than typical OCT imaging fields of view), we show that an order-of-magnitude improvement in three-dimensional (3-D) MM-OCT imaging speed can be achieved by rapid acquisition of a volumetric scan during the activation of the coil. Furthermore, we show volumetric (3-D) MM-OCT imaging over a large imaging depth range by combining this volumetric scan scheme with full-range OCT. Results with tissue equivalent phantoms and a biological tissue are shown to demonstrate this technique. © 2014 Society of Photo-Optical Instrumentation Engineers (SPIE) [DOI: 10.1117/1.JBO.19.12.126001]

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In this paper, we first discuss the operating factors that determine the MM-OCT data acquisition speed and then demonstrate an order-of-magnitude improvement in the imaging speed for the acquisition of a 3-D MM-OCT dataset using a modified scanning scheme. This is achieved by acquiring a volumetric scan at the maximum camera line-scan rate while applying the magnetic modulation cycles along the slow-scanning axis. Furthermore, we show that this volumetric scan scheme can be combined with other phase modulation techniques, such as full-range OCT, by applying a linear-phase modulation along the orthogonal-scan axis, which allows us to decouple the fast-axis modulation from the slow-axis modulation.
2 Methods

2.1 MM-OCT Image Acquisition Time

A number of valid scanning schemes can be used for MM imaging under harmonic excitation. The simplest and the most intuitive scan scheme is taking M-mode measurements (A-lines collected as a function of time) at several spatial locations. However, depending on the number of modulation cycles in each M-mode, this scheme substantially increases the imaging time, results in a large amount of acquired data, and requires continuous sinusoidal modulation, which will heat up the coil. Moreover, the transients arising due to the settling time of the galvanometers limit the speed at which data can be acquired. One alternate scheme utilized in dynamic OCE and MM-OCT, as shown in Fig. 1(a), is performed by modulating the magnetic field along time (t) with frequency $f_B$ while continuously scanning along the transverse dimension (x) with a lateral scan velocity ($v_x$) given by $v_x = f_s x_{fov}/N$, where $x_{fov}$ is the lateral field of view, $f_s$ is the sampling rate, and N is the number of A-scans within a cross-sectional image. Ideally, the scanning distance of the optical beam during one modulation cycle ($t_B = 1/f_B$) should be less than the transverse resolution ($\Delta x$) of the OCT system, i.e., $v_x t_B < \Delta x$. In addition, a high degree of spatial oversampling is required to ensure the separation of the structural image from the MM signal, while high temporal sampling ensures sufficient sampling of the modulation frequency and prevents phase-wrapping problems. These requirements impose constraints on the sampling rate $f_s$, modulation frequency $f_B$, lateral field of view ($x_{fov}$), and the imaging time (proportional to the number of modulation cycles $N_c$), and can be expressed as $mf_B < f_s < c f_B$, where $m$ is the temporal oversampling factor (number of A-lines per modulation cycle given by $f_s/f_B$, $m = 2$ for Nyquist criteria) and $c$ is defined as the spatial oversampling factor (number of A-scans per transverse resolution element), given by $c = \Delta x N/x_{fov}$. The mechanical properties of the sample and the OCT imaging parameters govern the operating frequency regime and the optimum number of modulation cycles required during MM-OCT imaging. The choice of the modulation frequency $f_B$ is dependent upon the tissue geometry and viscoelastic properties, and it is preferable to operate near the mechanical resonance frequency of the sample to attain the maximum sensitivity of the MM response. Considering the typical physical dimensions of the samples used and the range of elastic moduli ($E = 0.1$ to 1000 kPa) of biological soft tissues of interest, the samples exhibit mechanical resonances at frequencies <1 kHz. On the other hand, alternating magnetic field of higher frequencies (>10 kHz) should be avoided for imaging purposes as they can induce hyperthermia due to heating of the magnetic particles.

The upper constraint given by $f_s < c f_B$ prevents the use of high sampling rates [which is equivalent to the line-scan rate in the scheme shown in Fig. 1(a)]. As $f_B$ is generally fixed for a given sample, higher line-scan rates can only be used by either excessive spatial oversampling, reducing the field of view $x_{fov}$, or decreasing the number of modulation cycles within the imaging time window. For a typical modulation frequency of 100 Hz, $x_{fov} = 2.5$ mm, $\Delta x = 16$ $\mu$m, and $N = 4000$, the corresponding line-scan rate $f_s$ has the limits 200 < $f_s$ < 2560 Hz, which is much less than the capabilities of current OCT systems.

![Fig. 1](https://example.com/fig1.png)

**Fig. 1** Scanning scheme used in (a) conventional B-mode magnetomotive optical coherence tomography (MM-OCT), where $N_c$ is the number of modulation cycles that are acquired per fast axis frame. Before the acquisition of the next frame, a certain wait time (highlighted in blue) is given for cooling of the coil. During this wait time, a fast-axis frame with the magnetic field off can also be acquired. (b) Volumetric MM-OCT, where a number of fast-axis frames are acquired per modulation cycle, resulting in an order-of-magnitude increase in MM-OCT data acquisition speed.
which can have line-scan rates of up to several hundred thousand A-scans per second.\textsuperscript{16}

A more optimal scanning scheme with substantially reduced imaging time can be devised as shown in Fig. 1(b), which leverages the fast line-scan rates possible by current generation OCT systems. This scan scheme requires the electromagnetic coil to have sufficient magnetic field strength to cover the entire imaged tissue volume. In this scheme, the harmonic modulation is applied along the slow-time axis while a number of fast-axis frames are acquired per modulation cycle, resulting in an order-of-magnitude decrease in MM-OCT data acquisition time. The data processing for the volumetric MM-OCT is very similar to that described previously\textsuperscript{3} with the main difference being that the phase differences are now computed between successive fast-axis frames rather than successive A-scans.

### 2.2 Experimental Setup

Figure 2 shows the setup for volumetric MM-OCT. A 1310 nm spectral-domain OCT system with a superluminescent diode (LS2000B, Thorlabs) with 170 nm bandwidth was used as the light source. The measured axial and transverse resolutions (full width at half maximum) of the system were 6 and 16 μm, respectively. A 1024-pixel InGaAs line-scan camera (SU-LDH2, Goodrich) operating at a line-scan rate of 92 kHz was used in the spectrometer with an optical imaging depth of 2.2 mm. The phase noise of the system measured with a static sample placed in the sample arm was $\sim 180$ milli-radians along the slow axis and $\sim 20$ milli-radians along the fast axis. A solenoid coil was placed in the sample arm for magnetic modulation. The magnetic field strength generated by the coil was measured to be $\sim 150$ Gauss at a distance $\sim 1$ cm away from the coil. On activation of the coil, the magnetic particles undergo displacements in the direction of the magnetic field gradients and the optical path length changes induced by these small-scale displacements are measured using phase-resolved processing methods. A mirror mounted galvanometer was placed in the reference arm for the full-range modulation while the waveforms shown in Fig. 2(b) were used for driving the system.

### 2.3 Phantom Preparation

In order to show the merits of the proposed technique, we prepared samples with the magnetic particles present in a localized region within a 3-D field of view imaged using OCT. Tissue-mimicking phantoms were prepared by mixing polydimethylsiloxane (PDMS) fluid with the curing agent RTVA and cross-linker RTVB (with the ratios 100:10:1, PDMS:RTVA:RTVB). Titanium dioxide scattering particles (size $< 5 \mu m$, 0.5 mg/ml) were added to the mixture to increase the optical scattering and the solution was sonicated for 1 h. A small amount of microspheres ($25 \mu L/ml$) that contained magnetic nanoparticles ($Fe_3O_4$, size 50 to 100 nm)\textsuperscript{4} were then added, and subsequently, the mixture was left in the oven for 8 h at 80°C for curing.

### 3 Results

#### 3.1 Influence of Scanning Parameters on MM-OCT Signal

We first investigated the influence of different scanning parameters on the MM signal under a harmonic excitation waveform. These measurements were performed on a PDMS-based phantom containing a uniform concentration of magnetic nanoparticles (MNPs). In Fig. 3(a), the dependency of the MM...
Fig. 3 Effect of the scanning parameters on MM signal levels. (a) MM signal as a function of an increase in the temporal oversampling factor. M-mode measurements were taken at a single spatial location with different number of modulation cycles (\(N_c\)). (b) MM signal as the number of modulation cycles per resolution element is increased. B-mode images were acquired with a lateral field of view of 1.5 mm and MM signal values were calculated for each spatial location. The MM signal (dB) values shown correspond to the mean value of the MM signal obtained from each B-mode image.

Fig. 4 Volumetric MM-OCT results. (a) Volume rendered OCT processed dataset of a PDMS-based phantom. The lateral dimensions of the volume are 3.2 mm \(\times\) 3.2 mm, while the optical length along depth is 2.2 mm. (b) Volume rendered MM-OCT processed dataset showing the presence of magnetic microspheres. (c) Volume rendered OCT processed dataset (2 mm \(\times\) 2 mm \(\times\) 2.2 mm) of human adipose tissue with an embedded tumor mimicking PDMS-based inclusion. (d) Volume rendered MM-OCT dataset with the inclusion giving the MM-OCT signal.
response on M-mode data acquired with different temporal over-
sampling factors \((m)\) and number of modulation cycles \((N_c)\) is
shown. The MM signal (dB) values were computed from the
mean power spectrum (obtained after averaging the power spec-
trum along depth) of the acquired M-mode data at a modulation
frequency of 100 Hz. The values reported are obtained by sub-
tracting the peak values (in dB) at the modulation frequency
from the baseline noise floor in the adjacent frequency
bands. As expected, the MM signal improves by increasing
\(N_c\) while an increase in \(m\) improves the MM response up to
the point where it is sufficiently sampled to prevent any
phase-wrapping problems. The choice of \(m\) should at the mini-
mum satisfy the Nyquist criteria while \(m > 6\) is desirable for
optimal results. However, a higher temporal oversampling fac-
tor may be needed if the displacements are large to prevent any
phase-wrapping problems and for more accurate phase lag esti-
mates. In Fig. 3(b), the effect of scan speed and the number of
modulation cycles per transverse resolution element on the MM-
OCT signal is shown. B-mode data over a lateral scan range of
1.5 mm were acquired and the number of modulation cycles
\((N_c)\) within the imaging time window was varied by changing
the number of A-scans (over a fixed lateral scan range) while
keeping the sampling rate \((F_s)\) constant. This will increase
both the spatial oversampling factor \((c)\) and the number of
modulation cycles \((N_c)\) within the image. As mentioned previ-
ously, at least one modulation cycle per resolution element is
highly desirable; however, as the plot in Fig. 3(b) suggests,
increasing the number of modulation cycles per transverse
resolution element increases the MM SNR as averaging over
spatial locations having uniform motion can enhance the sensi-
tivity. We also note that at higher sampling rates \((F_s)\), the
MM-OCT signal level improves, which is possibly due to a
reduction in the phase noise of the system at higher scan rates.

These plots point out an inherent tradeoff between the imag-
ing time and MM sensitivity, as was alluded to in the previous
section. The plots suggest that the larger the number of modu-
lation cycles and the higher the temporal and spatial oversam-
factors, the greater the MM sensitivity, but at the expense
of an increased imaging time.

### 3.2 Volumetric MM-OCT

Volumetric MM-OCT datasets using tissue-mimicking phan-
toms and human adipose tissue are shown in Fig. 4. These data-
sets were acquired using a maximum camera line-scan rate of
92 kHz at 300 frames per second (fps) using the modified
scan scheme shown in Fig. 1(b). The magnetic modulation fre-
cuency of 50 Hz was applied, giving a temporal oversampling
factor of 6. The lateral pixel dimensions were 256 and 2048
along the fast and slow axes, respectively, with a total volume
acquisition time of \(\sim 7\) s, which corresponds to 340 modulation
cycles. The same dataset, if acquired with the traditional
MM-OCT scan scheme [Fig. 1(a)], would have required
\(\sim 30\) min (excluding the time it would require for the coil to
cool down during imaging). Hence, our results demonstrate
a significant reduction (\(\sim 250\) times) in the acquisition time.
Figures 4(a) and 4(b) show volume-rendered datasets of
a PDMS-based phantom acquired over a transverse field of
view of \(3.2\) mm \(\times 3.2\) mm. Standard OCT processing was per-
formed to obtain the dataset shown in Fig. 4(a), where a corner
cut through the volume shows the microsphere inclusion within
the sample. The presence of the magnetic microsphere inclusion
is clearly revealed after MM-OCT processing in Fig. 4(b), where

![Fig. 5 Full-range volumetric MM-OCT. (a) Processing steps. (b) Lateral Fourier transform of the fast-axis
frame showing the shift in frequency due to the linear-phase modulation along the fast axis. The high-
lighted region corresponds to the filtered region. (c) Lateral Fourier transform of the phase differences
along the slow axis showing the peak corresponding to the magnetic modulation frequency. The high-
lighted region corresponds to the band-pass filter bandwidth.](https://ebooks.spiedigitallibrary.org/journals/Journal-of-Biomedical-Optics)
only the region that corresponds to the presence of microspheres gives a strong MM-OCT signal within the PDMS phantom. The MM-OCT volume in Fig. 4(b) was obtained by further processing the OCT dataset by calculating phase differences between adjacent A-scans along the slow-axis frames and filtering the signal corresponding to the magnetic modulation frequency of 50 Hz. Subsequently, a two-dimensional median filtering operation was done on each frame to remove any residual noise.

In Figs. 4(c) and 4(d), we show an ex vivo human adipose tissue dataset containing an artificially embedded inclusion mimicking the presence of a tumor within the normal tissue. The inclusion was cut from a PDMS-based phantom containing a relatively high concentration of MNPs (2 mg/ml) and having a stiffness of ∼10 kPa. Figure 4(c) shows the OCT processed volume rendered dataset, while Fig. 4(d) shows the MM-OCT processed dataset that clearly shows that only the tumor-mimicking region gives an MM-OCT signal.

### 3.3 Full-Range Volumetric MM-OCT

Next, we combine the volumetric MM-OCT with full-range OCT by modulating a galvanometer-mounted mirror in the reference arm. The full-range OCT operation removes the conjugate image in spectral-domain OCT systems, enabling the utilization of the full imaging depth allowed by the spectrometer. This also allows higher sensitivity by placing the zero optical path length (OPL) inside the sample as the sensitivity degrades away from the zero OPL in spectral-domain OCT due to the finite spectral resolution of the spectrometer. The axial motion of the particles due to magnetic modulation can degrade the full-range reconstruction.\(^\text{17}\) In our experiments, we applied the sinusoidal modulation along the slow axis for the MM signal and linear-phase modulation along the fast axis for the full-range operation.\(^\text{18,19}\) Similar utilization of the orthogonal scan axes has been used for combining full-range operation with optical microangiography.\(^\text{20}\) As only a fraction of the magnetic modulation cycle is completed during each fast-axis frame acquisition, the two modulations do not significantly influence one another. The full-range volumetric MM-OCT data were processed postacquisition and the processing steps are outlined in Fig. 5(a). After background subtraction and resampling of the raw spectrum, the full-range processing steps of the lateral Fourier transform (FFT), band-pass filtering, and inverse FFT are each performed for the fast-axis frames followed by an FFT along wavenumber \((k)\) for reconstructing full-range OCT.\(^\text{19}\) Subsequently, the MM processing is applied to all the slow-axis

![Fig. 6 Full-range volumetric results of a PDMS-based phantom with magnetic microspheres.](image)
frames as outlined in Fig. 5(a). Figure 5(b) shows the typical spectrum obtained after a lateral FFT is applied along the fast axis (x-direction) in full-range processing, while the plot in Fig. 5(c) shows the MM response by taking the FFT of the phase differences of adjacent A-scans along the slow axis. The dashed lines highlight the regions that are band-pass filtered.

Figure 6 shows the results of volumetric MM-OCT data acquisition combined with the full-range OCT, which enables us to obtain a total optical imaging depth of 4.4 mm. In Fig. 6(a), a cross-sectional plane of a PDMS phantom containing an inclusion of magnetic microspheres is shown. In spectral-domain OCT systems, the roll-off of the spectrometer decreases the sensitivity away from the zero OPL. Hence, the inclusion containing microspheres can be seen only faintly at an optical distance of ~1.8 mm beneath the top surface. If the phantom is placed close to zero OPL, the conjugate image overlaps with the original image as shown in Fig. 6(b). After applying the full-range operation, the conjugate image is removed, and the microsphere inclusion can now be clearly seen in Fig. 6(c). The lateral pixel dimensions in this dataset were 512 and 2048 along the fast and slow axes, respectively, over a 2 mm × 2 mm field of view. This dataset was acquired with an effective frame rate of 150 fps with an acquisition time of ~13.5 s. Figure 6(d) shows the full-range volumetric MM-OCT where, as expected, only the magnetic microspheres give a signal. The banding artifact seen in this cross-sectional image is most likely due to aliasing caused by the low temporal sampling. Figure 6(e) shows a volume rendered dataset, which clearly shows the presence of the microsphere inclusions within the OCT volume.

4 Discussion and Conclusion

In this paper, we have demonstrated an order-of-magnitude improvement in the data acquisition speed for volumetric MM-OCT and combined it with full-range OCT, enabling us to obtain measurements over a large imaging depth. This volumetric scan scheme relies on the electromagnetic coil to provide sufficient magnetic field strength over the entire tissue volume scanned with OCT. For better spatial localization, it might be desirable to use a focused magnetic field that can excite tissue regions smaller than the OCT imaging volume. However, designing highly spatially focused magnetic fields with sufficient strength is challenging, especially given the typically small OCT fields of view.

In volumetric MM-OCT, the temporal sampling rate along the slow axis is dependent on the frame rate of the system. Hence, a tradeoff exists between spatial sampling along the fast axis and the achievable system frame rate. The relatively low temporal sampling rate would make this technique more susceptible to phase-wrapping problems, limiting the dynamic range of the MM-OCT measurements. However, phase wrapping can be avoided by decreasing the voltage on the coil, increasing the distance between the coil and the sample, or by employing phase-unwrapping algorithms. This technique would substantially benefit from higher A-scan rates, which would allow the acquisition of large fields of view with both high spatial and temporal sampling along both the fast and slow axes, which may increase the sensitivity and dynamic range of MM measurements.

In the full-range dataset, we note some degradation in the image quality, which is due to a number of factors, including fringe washout, band-pass filtering, low spatial oversampling, and the small amount of OPL changes that we were able to induce through the galvanometer-mounted mirror in the reference arm. Many of these problems can be avoided by using higher line-scan rates and better system design.

The processing steps for both full-range and MM-OCT are primarily based on the FFTs and band-pass filtering that can be implemented in the graphics processing units for processing and displaying the volumetric MM-OCT in real time. In the future, the MM-OCT volumetric scan scheme can be combined with other phase modulation schemes, such as optical microangiography. This volumetric scheme might also be extended to catheter-based MM-OCT configurations, where, due to the pull-back and fast rotation of the catheter, the standard B-mode MM-OCT scan scheme cannot be easily implemented. Moreover, it can be used in other dynamic excitation methods that use sinusoidal excitation, such as dynamic OCE.

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References


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